

Pole placement based on derivative of states

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ABSTRACT

State feedback is one of the important concepts in control theory. There are well defined methods like Ackermann's formula and Bass-Gura formula to find required gain matrix (K) which place close loop poles at the desired location. Here, instead of states, derivative of states are used in order to find the suitable control law. One of the applications of this type of feedback is vibration suppression of mechanical systems where feedback signal is generally taken from an accelerometer. Effectiveness of the proposed method is shown by simulation.

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1. Introduction

When input is applied to a system, output comes out. Sometimes output is not as good as desired. Possible reasons may be slowness of response, stability problem or steady state errors (Chen, 2014; Ogata, 2010). In these cases, control is applied in order to make the response better. Fig. 1 shows a general schematic of a system:

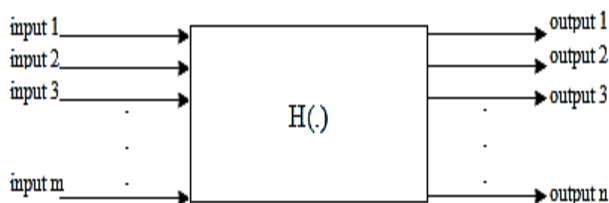


Fig. 1: General schematic of a multi input multi output system (MIMO)

Here, there are m inputs and n outputs. H is a set of differential equations (ODE) which govern the output response. When system response is not desired, a control system must be added to the original system in order to make the overall response better. In order to do this, two control techniques can be used:

1. Feedforward control,
2. Feedback control.

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It has been shown that feedback control has advantages over feedforward control (Ogata, 2010). Control problems can be divided into 2 groups (Chen, 2014; Ogata, 2010):

1. Tracking problems,
2. Regulation problems.

In tracking problems, goal is to follow a reference with minimal error. In regulation problems, system output must be kept at the desired level despite of disturbance and input changes.

In order to design a controller, either Laplace transform based methods or state space based methods can be used.

A lot of work has been done on pole placement problem by using state feedback (Valášek and Olgaç, 1999; Tuel, 1966). In this paper, pole placement problem is solved by *derivative* of state feedback.

2. State derivative based feedback control law

Assume a linear time invariant (LTI) system given by Eq. 1:

$$\dot{x} = Ax(t) + Bu(t) \quad (1)$$

$$A \in \mathbb{R}^{n \times n}, x(t) \in \mathbb{R}^n, B \in \mathbb{R}^n \text{ and } u(t) \in \mathbb{R}.$$

$x(t)$ is state vector and $u(t)$ is control input. Assume pair (A, B) is controllable, i.e. controllability matrix is full rank (Eq. 2).

$$u(t) = -K\dot{x}(t) \quad (2)$$

Eq. 2 uses derivative of states in order to produce control signal.

After putting (2) in (1), following equation is obtained (Eq. 3):

$$\dot{x} = (I + BK)^{-1}Ax(t) \quad (3)$$

Here, problem is to find gain matrix (K) such that close loop poles (Eigenvalues of $(I + BK)^{-1}A$) are desired set Δ_1 , given by $\Delta_1 = \{\lambda_1, \lambda_2, \dots, \lambda_n\}$. In order to solve the problem, following theorem is used.

Theorem 1: Assume A is an invertible matrix. Matrix A has Eigen values $\{\lambda_1, \lambda_2, \dots, \lambda_n\}$, if and only if Eigen values of matrix A^{-1} are $\{\lambda_1^{-1}, \lambda_2^{-1}, \dots, \lambda_n^{-1}\}$ (Strang, 2006). Inverse of $(I + BK)^{-1}A$ is found first (Eq. 4):

$$((I + BK)^{-1}A)^{-1} = A^{-1}(I + BK) = A^{-1} + A^{-1}BK = A_{new} + B_{new}K \quad (4)$$

where, $A_{new} = A^{-1}$ and $B_{new} = A^{-1}B$.

Assume a dynamical system as Eq. 5:

$$\dot{q} = A_{new}q + B_{new}W(t) \quad (5)$$

$W(t)$ is the control input for this new system. Assume $W(t)$ is chosen as (Eq. 6):

$$W(t) = -Kq(t) \quad (6)$$

using this control law Eq. 5 can be write as (Eq. 7):

$$\dot{q} = (A_{new} - B_{new}K)q(t) \quad (7)$$

If gain matrix K is chosen such that eigen values of $(A_{new} - B_{new}K)$ are $\Delta_2 = \Delta_1^{-1} = \{\lambda_1^{-1}, \lambda_2^{-1}, \dots, \lambda_n^{-1}\}$ then gain matrix K puts the eigenvalues of system in Eq. 1 at $\Delta_1 = \{\lambda_1, \lambda_2, \dots, \lambda_n\}$. So, problem of finding gain matrix K for derivative of state feedback control law in Eq. 2 can be solved by converting the problem to a new system of Eq. 5 and using a state feedback control law as Eq. 6.

3. Method for determining gain matrix K

In order to solve the state feedback control problem for new system of Eq. 5, (pole placement) there are well known methods like (Chen, 2014):

1. Ackermann's Method,
2. Bass-Gura Method.

These methods are studied with examples in Chen (2014). In this paper, Ackermann's method is used. Assume that (Eq. 8):

$$\alpha(s) = (s - \lambda_1^{-1})(s - \lambda_2^{-1}) \dots (s - \lambda_n^{-1}) = s^n + \alpha_{n-1}s^{n-1} + \dots + \alpha_0 \quad (8)$$

Ackermann (1972) has shown gain matrix K which places eigen values of close loop system in roots of $\alpha(s)$, i.e. $\{\lambda_1^{-1}, \lambda_2^{-1}, \dots, \lambda_n^{-1}\}$ is given by (Eq. 9):

$$K = q_n^T \alpha(A) \quad (9)$$

where, $q_n^T = [0, 0, \dots, 0, 1] \varphi_c^{-1}$ and $\varphi_c^{-1} = [B_{new}, A_{new}B_{new}, \dots, A_{new}^{n-1}B_{new}]$ is called controllability matrix.

4. An example

In order to show effectiveness of proposed method, an example is given. Assume the circuit shown in Fig. 1. State space model is given by (Eq. 10):

$$\begin{pmatrix} \dot{i} \\ \dot{V}_1 \\ \dot{V}_2 \end{pmatrix} = \begin{pmatrix} 0 & 0 & -\frac{1}{L} \\ 0 & -\frac{1}{R_1 C_1} & \frac{1}{R_1 C_1} \\ \frac{1}{C_2} & \frac{1}{R_1 C_2} & -\frac{1}{R_1 C_2} \end{pmatrix} \begin{pmatrix} i \\ V_1 \\ V_2 \end{pmatrix} + \begin{pmatrix} \frac{1}{L} \\ 0 \\ 0 \end{pmatrix} V_{in} \quad (10)$$

where, $[i, V_1, V_2]^T$ is state vector, i is inductor current, V_1 is capacitor C_1 voltage and V_2 is capacitor C_2 voltage. V_{in} is assumed as control input (Fig. 2).

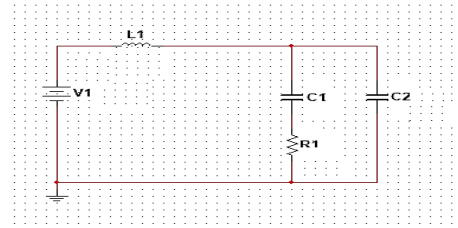


Fig. 2: Circuit for illustrative example

For simplicity we take $L_1 = 1H$, $C_1 = 1F$, $C_2 = 1F$ and $R_1 = 1\Omega$. With this values Eq. 10 can be rewritten as (Eq. 11):

$$\begin{pmatrix} \dot{i} \\ \dot{V}_1 \\ \dot{V}_2 \end{pmatrix} = \begin{pmatrix} 0 & 0 & -1 \\ 0 & -1 & 1 \\ 1 & 1 & -1 \end{pmatrix} \begin{pmatrix} i \\ V_1 \\ V_2 \end{pmatrix} + \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} V_{in} \quad (11)$$

Eq. 11 is controllable and has poles at $-1.755, -0.123 \pm 0.745j$. Assume Δ_1 , i.e. set of desired Eigen values, is given by (Eq. 12):

$$\Delta_1 = \{-3, -4, -5\} \quad (12)$$

after applying the aforementioned procedure $K = [10 \ 33 \ 26]$.

$$\text{So, } V_{in} = -[10 \ 33 \ 26] \begin{bmatrix} i \\ V_1 \\ V_2 \end{bmatrix} = -10i - 33V_1 - 26V_2$$

is the desired control law.

5. Simulation

In order to simulate the system Matlab® / Simulink® has used. Matlab® has great variety of tools in order to simulate dynamical systems. Fig. 3 shows simulink diagram of the example studied before.

Results (state variable of circuit: i, V_1, V_2) are shown in Fig. 4.

Fig. 4 shows that applying the control law given by $V_{in} = -10i - 33V_1 - 26V_2$ can force the system

to return to equilibrium point $[0, 0, 0]^T$, also close loop system has a more fast response than to original system. Although in simulation environments, all the variables are measurable easily, in a real life there are cases which only derivative of states can be obtained. For example in mechanical vibration suppression, usually an accelerometer is used as sensor and obtained states are velocity and acceleration not position and velocity. In order to solve these family of problems modification shown in these paper must be applied to formulas.

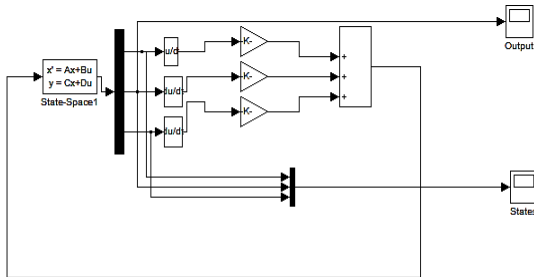


Fig. 3: Simulink diagram of studied example

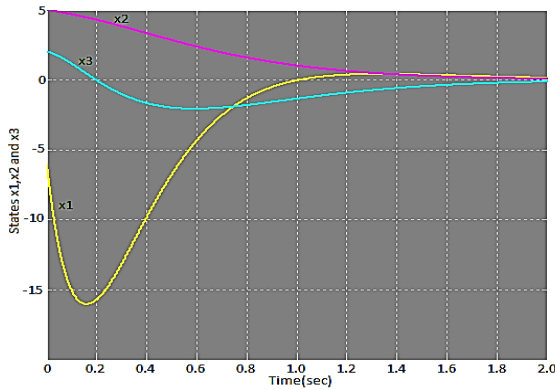


Fig. 4: Simulation results initial condition is $[-5, 5, 2]^T$

6. Conclusion

Pole placement problem is studied in recent decades by many researchers. In this paper, instead of states, derivative of states is used for placing poles at the desired location. A method is described for finding required gain matrix. Effectiveness of studied method is shown with an example.

Next step is to apply the studied method to an industrial application.

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